



## **XD1-L – Cable Differential Protection Relay**

**(March 2008)**

**Manual XD1-L (Revision New)**

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# 1. Application and features

Protection devices for electrical systems minimize fault damages, assist in maintaining power system stability and help to limit supply interruptions to consumers.

Line differential protection is a strict selective object protection. Within a very short time this relay detects faults occurring within the zone to be protected by comparing the currents flowing between two measuring points, for instance the current on either side of a line or cable. Faults detected instantaneously are :

- Short circuits between lines
- Insulation defects
- Earth-faults (at rigid or low-resistance neutral earthing)

Tripping must not occur at any other operational conditions (e.g. faults occurring outside the zone being protected).

For the protection of lines relay type XD1-L is available at a very competitive price. The basic version of this re-lay absolutely meets the requirements of differential protection outlined above.

The basic version of the relay can be extended even later by the addition of extra cards. By using a new method of evaluating current signals, the relay can determine whether C.T. saturation is due to internal or external faults and either trip or stabilize accordingly.

Thus this extended relay (type XD1-L SAT) is particularly appropriate for:

- Different sets of C.T.s
- Retrofitting
- Difficulty conditions
- High-quality items to protect
- High mains power
- Motor feeders

The relay XD1-L of the PROFESSIONAL LINE has the following special features:

- Fault indication via LEDs
- Extremely wide operating ranges of the supply voltage by universal wide-range power supply
- Very fine graded wide setting ranges
- Extremely short response time
- Compact design by SMD-technology
- Static, three-phase differential protection relay
- Dual slope percentage bias restraint characteristic with adjustable bias setting
- Applicable for 45 to 65 Hz
- Burden < 0.05 VA at rated current
- Setting ranges:
  - Differential current:  
10 to 85 %  $I_N$  in 16 steps
  - Bias slope:  
10 to 85 % of through current in 16 steps
- Isolation between all independent inputs
- High electromagnetic compatibility
- The use of precision components guarantees high accuracy
- Permissible temperature range: -20°C to +70°C
- According to the requirements of VDE 0435, part 303 and IEC 255
- Wire break supervision for C.T. lines

Extended version (type suffix SAT)

- Ability to recognize saturation of the main current transformers
- Extremely stable even during saturation of current transformers
- Additional printed circuits for recognition of saturated C.T.s can be added at a later stage, e.g. as the power system develops and fault levels increase

Further features of the unit XD1-L:

- High reliability and easy-to-service arrangement
- Plug in design makes it possible to simplify extension of the basic unit
- LED indication of the operating conditions
- Automatic supervision of bias current connections

## 2. Design

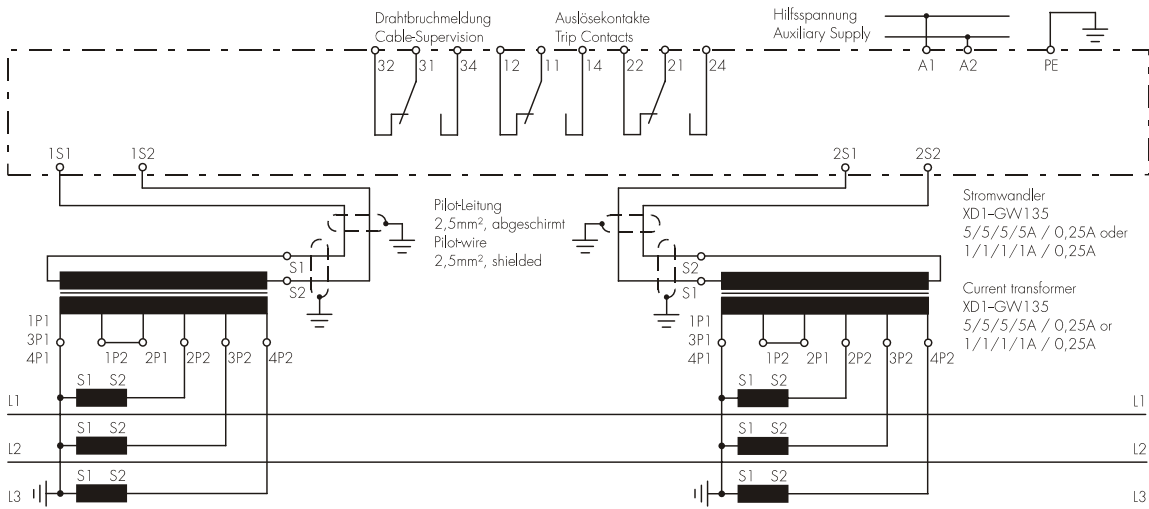


Figure 2.1: Connection diagram

### Auxiliary voltage supply

Unit XD1-L needs a separate auxiliary voltage supply. Therefore a DC or AC voltage must be used. Unit XD1-L has an integrated wide range power supply. Voltages in the range from 19 - 390 V DC or 35 - 275 V AC can be applied at connection terminals A1 and A2.

### Summation C.T.

The three C.T.s for each line are connected to a three-phase summation C.T. (type XD1-GW135, which is provided for each order). So the three C.T. currents are combined to a characteristic single-phase alternating current. There are only two auxiliary wires needed for supervision of measuring signals. This kind of differential protection is used for lines up to 1500 m. By internal electronics the pilot lines are supervised for wire breaks. In case of wire break or supply failure, the supervision relay releases and closes contacts 31 - 32. At the same time the trip element is blocked.

### Contact positions

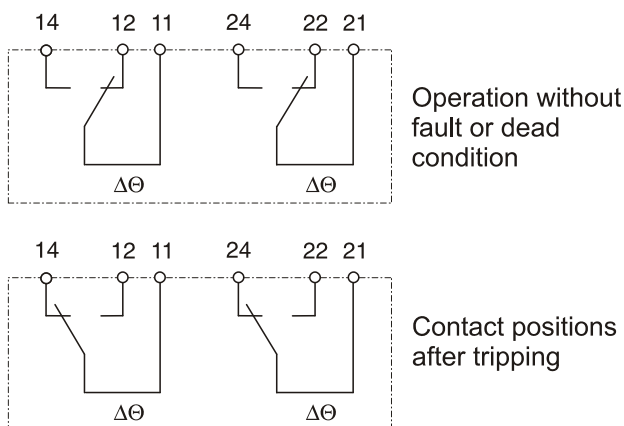


Figure 2.2: Contact positions of the output relays

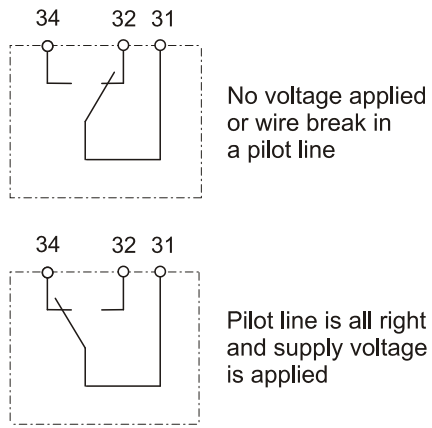


Figure 2.3: Contact positions of the indications relay

## 3. Working Principle

### 3.1 Operating principle of the differential protection

The fundamental operating principle of differential protection is based on a comparison of the current to the star point with the current to the busbar. For an ideal line the currents entering and leaving must be equal. Or according to Kirchhoff's first law "the vector sum of currents entering and leaving any point must be zero". If the sum  $I_d$  of currents is not zero, an internal fault is indicated.

The basic equipment of relay XD1-L recognizes these differential currents  $I_d$  and the relay gives the tripping command according to the precision measuring characteristic (see tripping characteristics).

To explain the function at XD1-L the working principle is shown in figure 3.1.

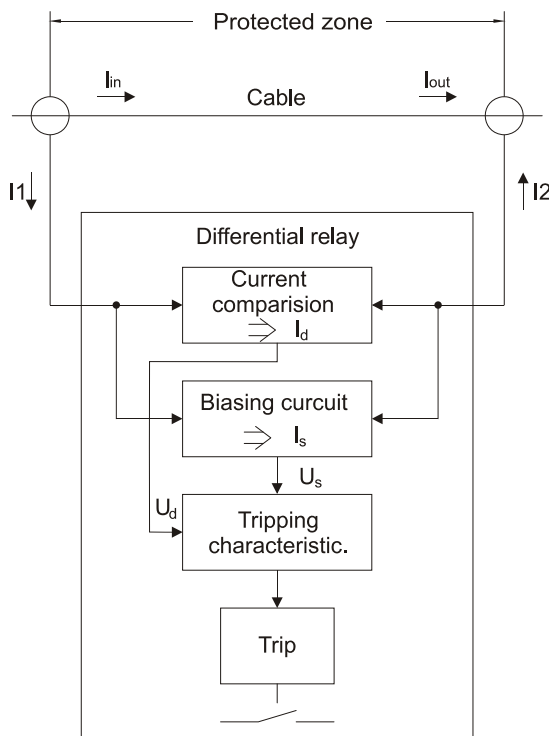


Figure 3.1: Working principle XD1-L  
 $I_d$  = differential (tripping) current  
 $I_s$  = stabilizing current



### 3.2 Working principle of the C.T. saturation detector SAT

With many differential protection systems, relay instability may cause to trip if the main current transformers saturate. In the transient condition of saturation the C.T.s on both ends of the protected zones do not produce the correct secondary current according to the primary current. The differential relay measures a differential current on the secondary C.T. side which is not present on the primary side. Hence a false tripping might occur.

Such transient phenomena causing C.T. saturation may occur due to:

- Heavy through faults (external short circuit)
- Starting of big motors
- Magnetizing inrush currents of transformers

The figure 3.2 explains the saturation of the C.T. core due to a short circuit current. In the instant of a short circuit often a DC-component is present in the current. The high primary current induces a flux in the C.T. core, reaching the saturation level. The iron-core retains the high flux level even after the primary current falls to zero. In the time periods of saturation the C.T. does not transform the primary current to the secondary side but the secondary current equals zero.

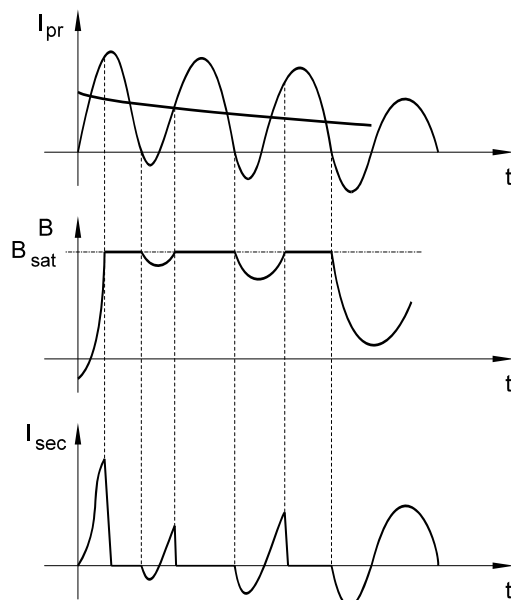


Figure 3.2      *Current transformer saturation*  
 $I_{pr}$  = Primary current with DC offset  
 $B_{sat}$  = Saturation flux density  
 $I_{sec}$  = Secondary current

Dissimilar saturation in any differential scheme will produce operating current.

Figure 3.3 shows the differential measurement on the example of extremely dissimilar saturation of C.T.s in a differential scheme. Figure 3.3 shows the secondary current due to C.T. saturation during a fault (internal fault). The differential current  $i_d$  represents the fault current. The differential relay must trip instantaneously.

Figure 3.3 shows the two secondary currents in the instant of an heavy external fault, with current  $i_1$  supposed to C.T. saturation, current  $i_2$  without C.T. saturation.

The differential current  $i_d$  represents the measured differential current, which is an operating current. As this differential current is caused by an external fault and dissimilar saturation of the two C.T.s, the differential re-lay should not trip.

Left:	Internal fault, Single end fed
	$i_1$ = secondary output current from saturated C.T. (theoretical)
	$i_2$ = 0; Internal fault fed from side 1 only.
	$i_d$ = measured differential current
Right:	External fault:
	$i_1$ = as in fig. 3.3 for an internal fault
	$i_2$ = normal current from C.T. secondary on side 2
	$i_d$ = measured differential current

The wave forms for the differential current  $i_d$  for internal and external faults are seen to be different for the cases considered.

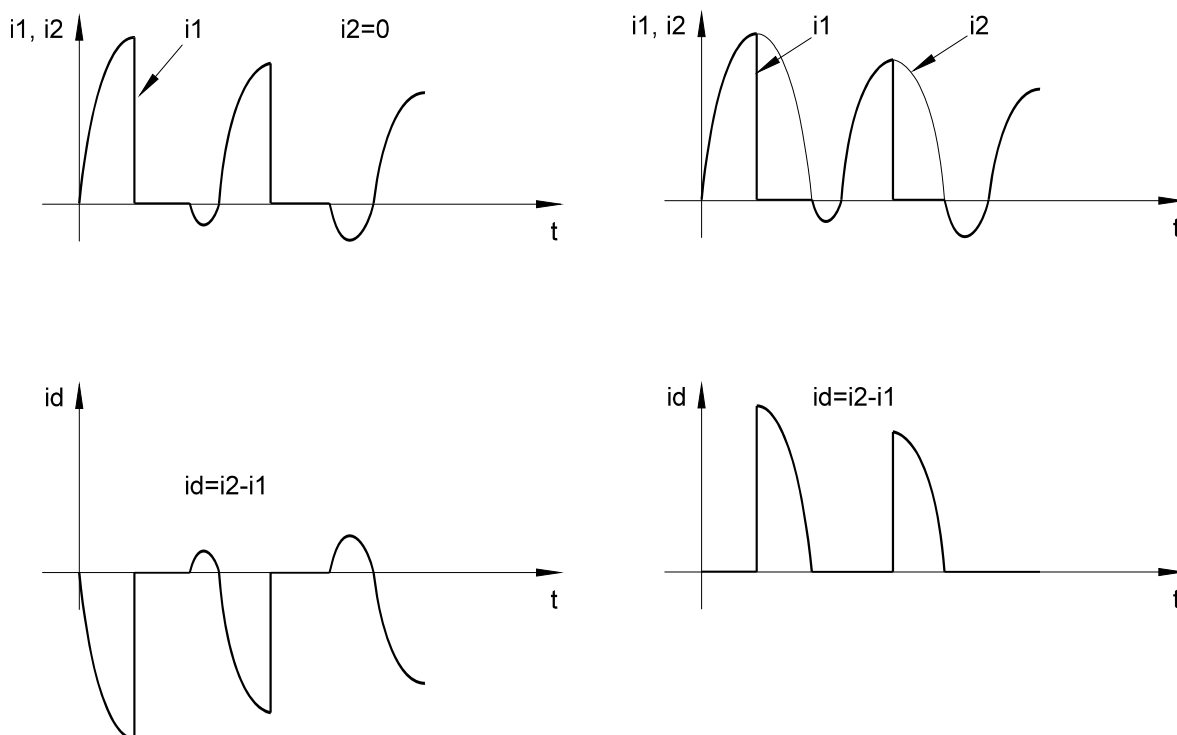


Figure 3.3: Current comparison with C.T.s saturated by DC offset in fault current wave form

The saturation detector SAT analyses the differential current of each phase separately. The SAT module differentiates the differential current and detects:

- Rate of change of differential current  $d(i_d)/dt$
- Sign of  $d(i_d)/dt$
- Internal/external fault
- Time period of saturation, within one cycle
- DC or AC saturation

The instant of an extreme rate of change of differential current  $d(i_d)/dt$  clearly marks the begin of a C.T. saturation.

The sign of this  $d(i_d)/dt$  value distinguishes the internal fault from an external fault.

One detected extreme  $d(i_d)/dt$  value per cycle indicates a saturation due to DC-current contents.

Whereas two extreme  $d(i_d)/dt$  values per cycle indicate a C.T. saturation caused by a high alternating current.

- The logic control evaluating above information derives:
- Only external faults lead to blocking of the trip circuit.
- In case of detected DC-current saturation the differential current measurement is blocked completely until: the transient condition ends, or an internal fault is detected (instantaneously), or AC-current saturation is detected.
- In case of detected AC-current saturation only the time periods of saturation are blocked during one cycle. This means that even under severe saturation the differential relay evaluates the differential current in „sound“ time periods. This is a major advantage to relays solely applying harmonic filters for saturation detecting.
- All detected transient phenomena change the tripping characteristic to the "coarse tripping characteristic" (pl. ref. to Technical Data).

### 3.3 Block diagram

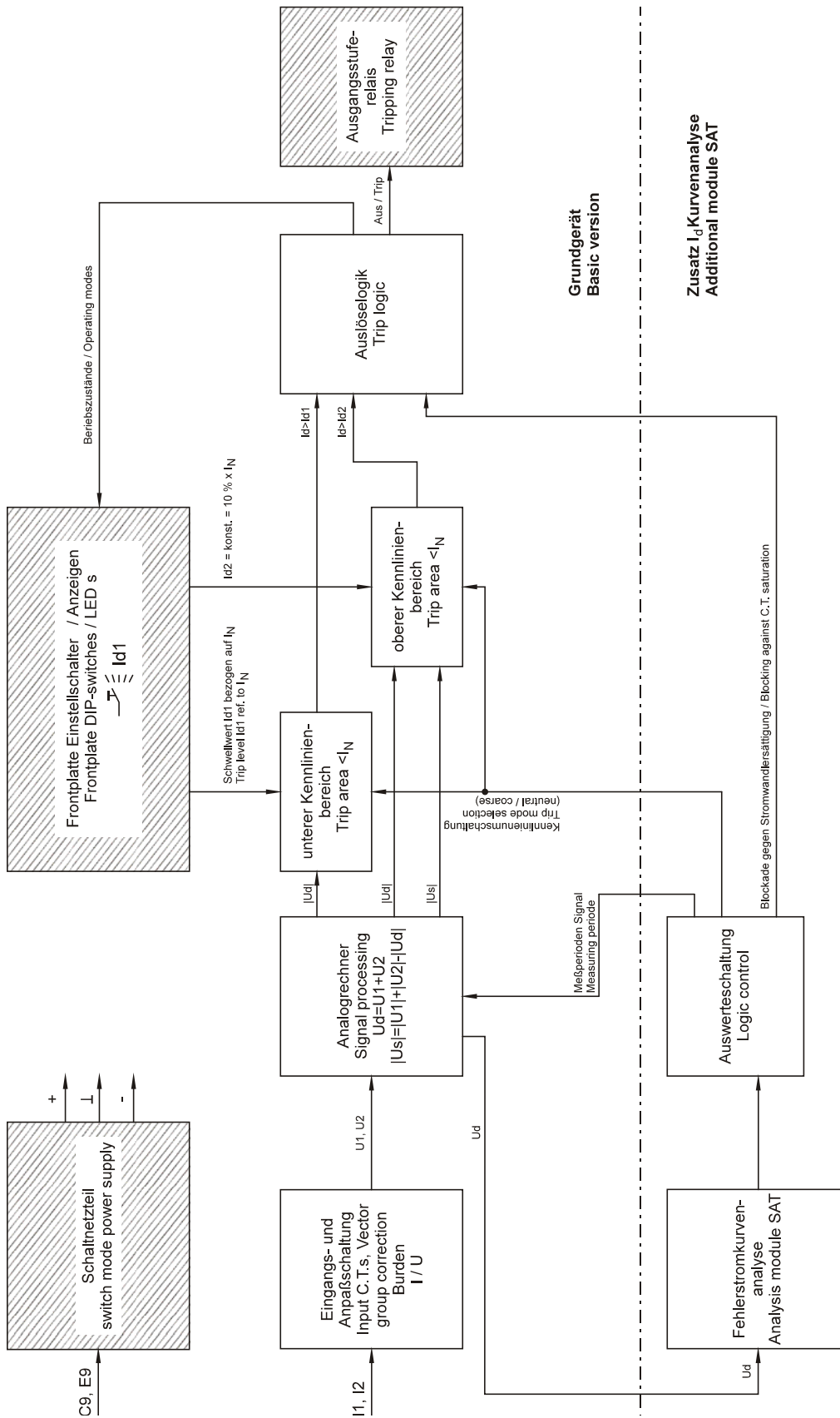


Figure 3.4: Block diagram

## 4. Operation and settings

All operating elements needed for setting parameters are located on the front plate of the XD1-L as well as all display elements.

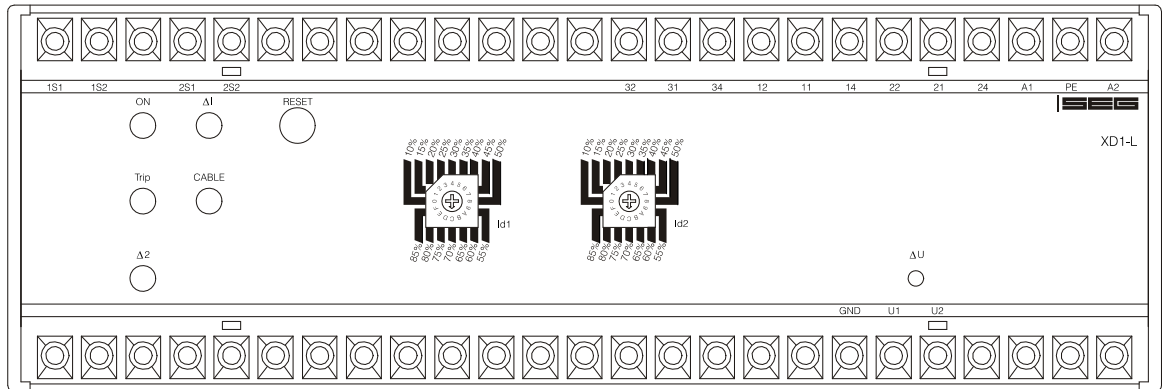


Figure 4.1: Front plate XD1-L

For adjustment of the unit the transparent cover has to be opened as illustrated. Do not use force! The transparent cover has two inserts for labels.

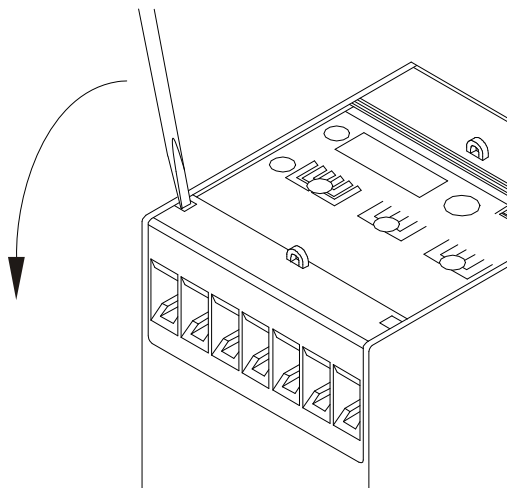


Figure 4.2: How to open the transparent cover

### LEDs

LED „ON“ is used for display of the readiness for ser-vice (at applied auxiliary voltage  $U_v$ ). LEDs  $\Delta I$  and TRIP are provided for fault indication. LED  $\Delta 2$  indicates changeover to the coarse measuring element (only with an additional SAT module).

If there is no wire break in the pilot lines and they are correctly connected, LED CABLE lights up green.

### Reset push button

The Reset push-button is used for acknowledgement and resetting the LEDs after tripping.

### Potentiometer

The potentiometer  $\Delta U$  on the lower right side of the front plate is provided for adjustment of the interposing C.T.s.

## 4.1 Parameter setting

For each phase the relay calculates the differential current  $I_d$  and the stabilizing current  $I_S$ . The differential current  $I_d$  is the vector difference between star point and outgoing currents. The value of differential current at which the relay responds is dependent on the stabilizing current, as shown in chapter 6.2 "Tripping characteristic".  $I_N$  is relay rated current (1 A or 5 A) and the two quantities  $I_d/I_N$  and  $I_S/I_N$  are scaled in multiples of rated current.

The basic version of the relay is equipped with the "fine" tripping characteristic only. The differential current  $I_d$  is adjustable from 10 - 85 % of rated current. With the extended version the tripping characteristic can be automatically switched from the selected "fine" to the fixed "coarse" characteristic.

The biased slope characteristic (right and upper part of the characteristic) prevents incorrect operation of the re-lay at through faults. The lower section of the characteristic shows the minimum differential current required to operate the relay with zero or low levels of stabilizing current.

Bias characteristic setting (related to stabilizing current  $I_S$ )       $I_{d2} \% = I_d/I_S = 10 - 85 \%$   
 Differential current settings (related to relay rated current  $I_N$ )       $I_{d1} \% = I_d/I_N = 10 \% \dots 85 \%$

The minimum differential current at which the relay picks up is defined by the lower section of the characteristic. For stability during transient conditions with extended version (SAT) of the relay the protection automatically changes over to the fixed "coarse" tripping characteristic. In this case the following settings apply:

Bias setting (related to  $I_S$ ):                       $I_{d2} \% = I_d/I_S = 120 \%$   
 Differential setting (related to  $I_N$ ):               $I_{d1} \% = I_d/I_N = 200 \%$

The relay has a stepped tripping characteristic:

- For differential currents  $I_d/I_N < 200 \%$  the time delay is 100 ms.

For differential currents  $I_d/I_N > 200 \%$  the relay trips instantaneously (approx. 40 ms).

## 4.2 Setting of the pickup value for the differential current $I_{d1}$ and $I_{d2}$

The pickup value of the differential current  $I_{d1}$  and  $I_{d2}$  can be adjusted by means of the step switch  $I_{d1}$  and  $I_{d2}$  in the range from 10 - 85 %. (Scale 5 %).

**Example:**

Adjustment of the characteristic is shown on the following diagram:

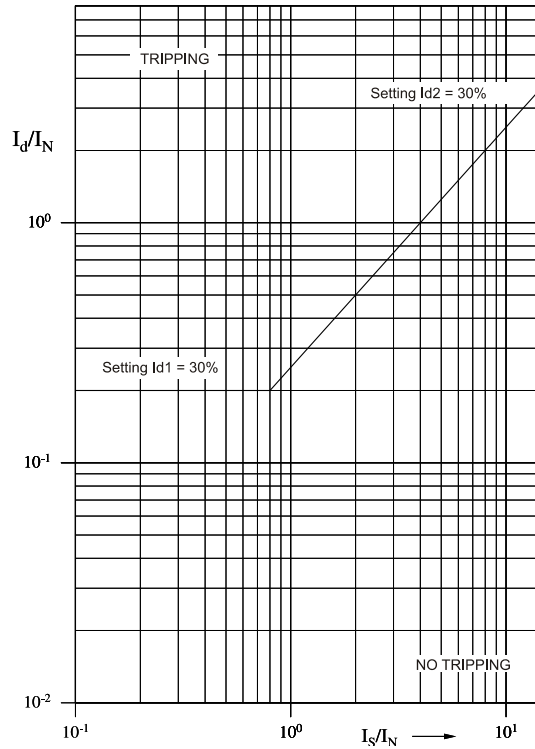


Figure 4.3: Diagram tripping characteristic

For this step-switch for  $I_{d1}$  has to be in the following positions:

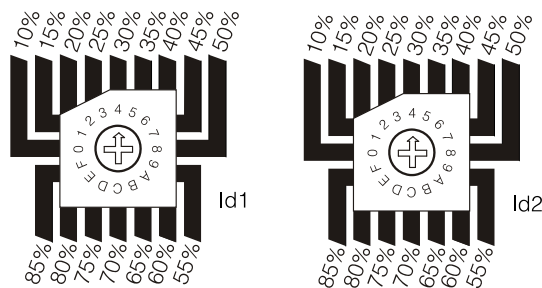


Figure 4.4: Adjustment of step switch

## 5. Relay testing and commissioning

The following test instructions should help to verify the protection relay performance before or during commissioning. To avoid a relay damage and to ensure a correct relay operation, be sure that:

- the auxiliary power supply rating corresponds to the auxiliary voltage on site
- the rated voltage corresponds to the plant data on site,
- the current transformer circuits are connected to the relay correctly
- all control- and measuring circuits as well as the out-put relays are connected correctly.

### 5.1 Connection of the auxiliary voltage

#### NOTE!

Prior to switch on the auxiliary power supply, be sure that the auxiliary supply voltage corresponds with the rated data on the type plate.

When the auxiliary power supply is switched on (terminals C9/E9) please observe that the LED "ON" is alight.

### 5.2 Checking the set values

Due to a check of the DIP-switch positions, the actual thresholds can be established. The setting values can be corrected, if necessary by means of the DIP-switches.

### 5.3 Secondary injection test

#### 5.3.1 Test equipment

- Ammeter, class 1 or better,
- Auxiliary voltage supply corresponding to the nominal auxiliary voltage of the device
- Single-phase AC supply (adjustable from 0 -  $1 \times I_N$ )
- Timer for the measuring of the trip delays
- Switching device
- Test leads and tools

#### NOTE!

Before this test is initiated by means of secondary current, it must be ensured that the relay cannot cause any switching actions in the system (shut-down risk).

#### 5.3.2 Checking of the pickup and dropout value

When checking the pickup value for  $I_{d1}$ , the analog input signals of the single phase alternating test current have to be fed to the relay via terminals 1S1 - 1S2.

When testing the pickup value, the alternating test current must first be lower than the set pickup value for  $I_{d1}$ .

Then the current will be increased until the relay picks up. The value that can be read from the Ammeter may not deviate by more than  $\pm 2.5\%$  of the setting value  $I_{d1}$ . The tripping values  $I_{d1}$  for the other current inputs should be checked accordingly.



### 5.3.3 Checking the trip delay

For checking the tripping time (time element of the relay), a timer is connected to the contact of the trip relay.

The timer has to be started simultaneously with connection of the test current and must be stopped when the relay trips.

## 5.4 Primary injection test

Generally, a primary injection test could be carried out in the similar manner as the secondary injection test above. Since the cost and potential hazards are very high for such a test, primary injection tests are usually limited to very important protective relays in power system.

### 5.4.1 Adjustment of the interposing C.T.s

The correct connection and accurate adjustment of the C.T.s can be checked with a voltmeter. For this 3 terminals are provided at the lower terminal strip. The associated adjustment potentiometers are arranged above these terminals. Differences of the main C.T.s up to 15 %  $I_N$  can be adjusted by the potentiometers.

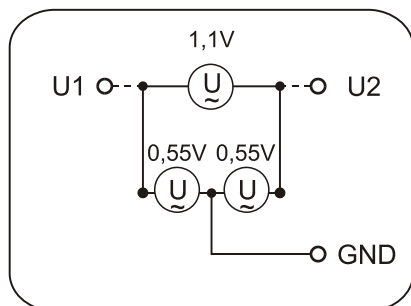


Figure 5.1: Connection of voltmeter

Information about measuring results can be found on the following table.

a)	Measuring 1 (U1 - GND) Measuring 2 (U2 - GND) Measuring 3 (U1 - U2)	550 mV 550 mV 1100 mV	Correct connection
b)	Measuring 1 (U1 - GND) Measuring 2 (U2 - GND) Measuring 3 (U1 - U2)	550 mV 550 mV 0 mV	Current flow of a C.T. (S1 and S2) is mixed-up
c)	Measuring 1 (U1 - GND) Measuring 2 (U2 - GND) Measuring 3 (U1 - U2)	550 mV 550 mV 550 mV	Phase position mixed-up (e.g. one current from phase L1, the other one from phase L2)
d)	Measuring 1 U1 - GND) Measuring 2 (U2 - GND) Measuring 3 (U1 - U2)	550 mV 550 mV 950 mV	Current flow and phase position of a C.T. is mixed-up

The internal measuring voltages proportional to the input currents may be measured as follows. The measuring instrument should be a digital multimeter set to AC-voltage measurement, range 2.0 V. The readings stated below refer to nominal current of the transformer (referring to the order form). Any current value below may be calculated proportionally.

Please also note that due to the C.T. errors and the transformer magnetizing current the measured values might deviate up to 10% from the theoretical values.

Nominal load current of the transformer is generally transformed to the internal measuring voltage of 550 mV AC. Both amplitudes of the measuring voltages of one phase, e.g. U1 and U2, should be equal. The phase angle of the voltages of one phase, e.g. U1 and U2, must be 180 degrees.

In case there are deviations from the expected value please check all wiring to the relay. This check must include the connection of the primary C.T. side and the secondary side.

If the single ended measurements (e.g. U1 - GND) differ within one phase, e.g.:

U1 - GND: 400 mV

U2 - GND: 600 mV

U1 - U2: 1000 mV

but the differential measurement equals the sum of both the deviation may be balanced using the concerned potentiometer on the front plate.

## 5.5 Maintenance

Maintenance testing is generally done on site at regular intervals. These intervals vary among users depending on many factors: e.g. the type of protective relays employed; the importance of the primary equipment being protected; the users past experience with the re-lay, etc.

For static relays like XD1-L, maintenance testing will be performed at least once a year according to the experiences.

## 5.6 Function test

### Note:

To prevent unintended switching off of the lines to be protected, the tripping line should be disconnected and then after the check reconnected again.

After disconnection of the tripping line the differential protection can be checked. During this procedure the load current flowing through the lines should be at least 50 %  $I_N$ . This current value must be well above the Id1 setting value. Now a winding, e.g. S1 - S2 in phase L1, at the secondary side of the main C.T. is to be bridged at low-resistance at one end of the line.

### Caution:

Do not open the electric circuit. (Danger to Life). Be-cause the secondary winding is bridged, this current does not flow through the summation C.T. and so a considerable differential current develops, causing the differential protection to trip.

For this check any of the other phases can also be used.

## 6. Technical Data

### 6.1 Relay case

Relay XD1-L is designed to be fastened onto a DIN-rail acc. to DIN EN 50022, the same as all units of the PROFESSIONAL LINE.

The front plate of the relay is protected with a sealable transparent cover (IP40).

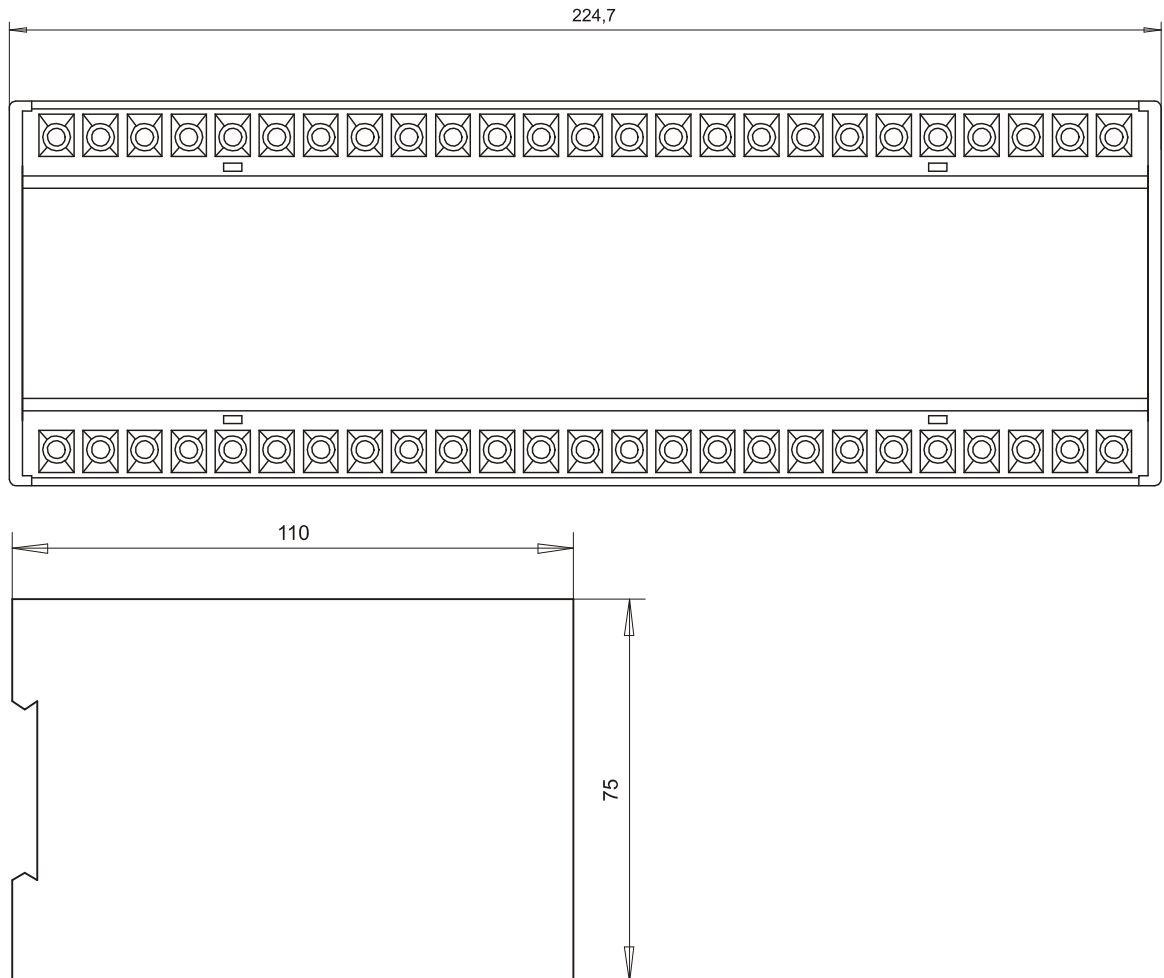


Figure 6.1: Dimensional drawing

#### Connection terminals

The connection of up to a maximum  $2 \times 2.5 \text{ mm}^2$  cross-section conductors is possible. For this the transparent cover of the unit has to be removed (see para. 3).

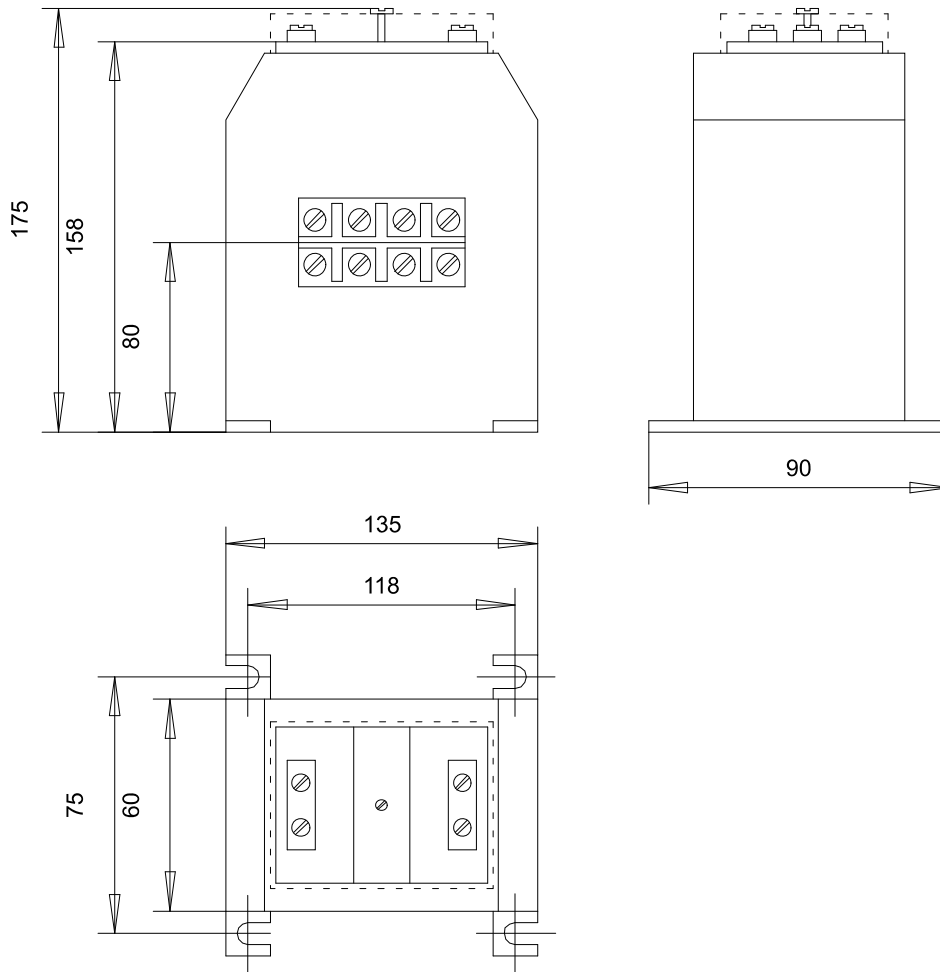


Figure 6.2: Dimensional drawing C.T. XD1-GW135

## 6.2 Technical Data

### Measuring input

Rated data:	
Rated current	1 A/5 A
Rated frequency $f_N$ :	50 - 60 Hz
Power consumption	
in current circuit:	at $I_N = 1 A$ < 0.1 VA
Thermal withstand capability	
in current circuit:	dynamic current withstand (half-wave)
	for 1 s 250 x $I_N$
	for 10 s 100 x $I_N$
	continuously 30 x $I_N$
	4 x $I_N$

### C.T.:

Type:	XD1-GW135
Design:	cast resign (winding)-C.T.
Transformation ratio:	5/5/5/0.25 A or 1/1/1/1/0.25 A
Power:	2 VA
Class:	5 P 10
Series:	0,8/3 kV
Frequency:	50/60 Hz
Diameter of wiring:	secondary wiring min. 2,5 mm <sup>2</sup>

### Auxiliary voltage

Rated auxiliary voltages $U_H$ :	35 - 275 V AC (f = 40 - 70 Hz)
	19 - 390 V DC

### General data

Dropout to pickup ratio:	> 97%
Returning time:	< 50ms
Returning time after tripping:	100ms $\pm$ 10ms
Minimum operating time:	30ms

### Output relays

The output relay has the following characteristics:

Maximum breaking capacity: 250 V AC / 1500 VA / continuous current 6 A

### For DC-voltage:

	ohmic	L/R = 40 ms	L/R = 70 ms
300 V DC	0.3 A/90 W	0.2 A/63 W	0.18 A/54 W
250 V DC	0.4 A/100 W	0.3 A/70 W	0.15 A/40 W
110 V DC	0.5 A/55 W	0.4 A/40 W	0.20 A/22 W
60 V DC	0.7 A/42 W	0.5 A/30 W	0.30 A/17 W
24 V DC	6.0 A/144 W	4.2 A/100 W	2.50 A/60 W

Max. rated making current:	64 A (VDE 0435/0972 and IEC 65/VDE 0860/8.86)
Making current:	min. 20 A (16 ms)
Mechanical life span:	30 x 10 <sup>6</sup> operating cycles
Electrical life span:	2 x 10 <sup>5</sup> operating cycles at 220 V AC / 6 A
Contact material:	silver cadmium oxide (AgCdO)

**System data**

Design standard:	VDE 0435, T303, IEC 255-4, BS142
Specified ambient service	
Storage temperature range:	- 40°C to + 85°C
Operating temperature range:	- 20°C to + 70°C
Environmental protection class F as per DIN 40040 and per DIN IEC 68, part 2-3:	relative humidity 95 % at 40°C for 56 days
Insulation test voltage, inputs and outputs between themselves and to the relay frame as per VDE 0435, part 303 and IEC 255-5:	2.5 kV (eff.), 50 Hz; 1 min
Impulse test voltage, inputs and outputs between themselves and to the relay frame as per VDE 0435, part 303 and IEC 255-5:	5 kV; 1.2/50 µs; 0.5 J
High frequency interference test voltage, inputs and outputs between themselves and to there lay frame as per IEC 255-6:	2.5 kV/1MHz
Electrostatic discharge (ESD) test as per VDE 0843, part 2 IEC 801-2:	8 kV
Radiated electromagnetic field test as per VDE 0843, part 3 IEC 801-3:	electric field strength 10 V/m
Electrical fast transient (Burst) test as per VDE 0843, part 4 IEC 801-4:	4 kV/2.5 kHz, 15 ms
Radio interference suppression test as per DIN/VDE 57871:	limit value class A

**Mechanical tests:**

Shock:	class 1 as per DIN IEC 255 part 21-2
Vibration:	class 1 as per DIN IEC 255 part 21-1
Degree of protection:	IP40 at closed front cover
Weight:	ca. 1.5 kg
Mounting position:	any
Relay case material:	self-extinguishing
Overvoltage class:	III

Technical data subject to change without notice!

Tripping characteristics

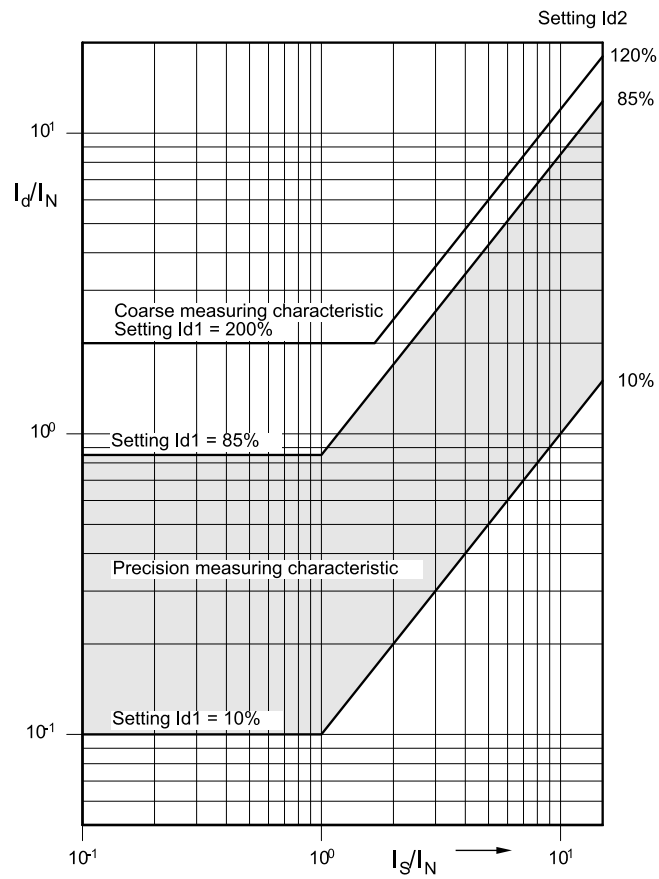


Figure 6.3: Tripping range

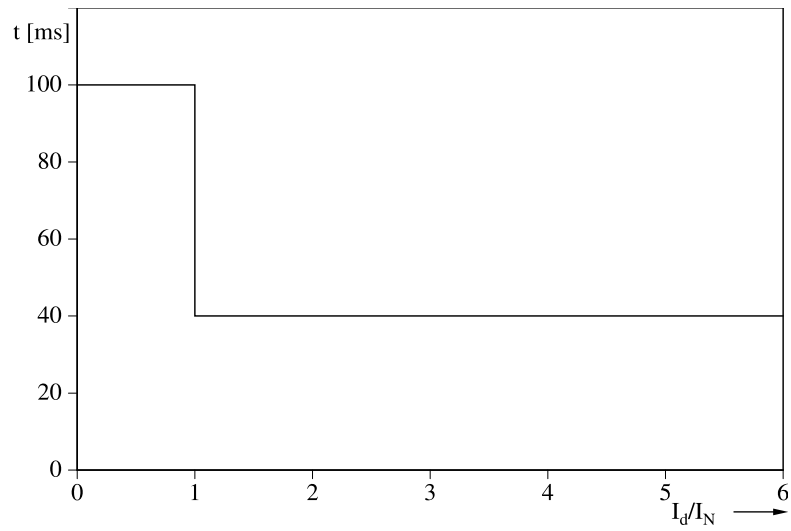


Figure 6.4: Tripping time

**Accuracy details**for  $I_S < I_N$ :

$$f = \left| \frac{I_{dAusl} - I_{dEinst}}{I_N} \right| \cdot 100\%$$

for  $I_S \geq I_N$ :

$$f = \left| \frac{I_{dAusl} - I_{dEinst}}{I_S} \right| \cdot 100\%$$

where

e = relative error

 $I_S$  = stabilizing current $I_N$  = rated current $I_{dtrip}$  = measuring differential current which results in tripping $I_{dset}$  = differential current setting**Note:**

The accuracy details quoted are based on interposing current transformer with exact correction ratio.

**Accuracy at reference conditions:**

- Temperature range -5°C...40°C  $e \leq 2.5 \%$
- Frequency range 50 Hz...60 Hz:  $e \leq 2.5 \%$

If the operating temperature or frequency are outside the ranges quote, additional errors are:

- Temperature range -20°C...70°C:  $e_{add} < 2.5 \%$
- Frequency range 45 Hz...66 Hz:  $e_{add} = 1 \%$



## 7. Order form

<b>Differential protection relay</b>		<b><i>XD1-</i></b>				
Line protection (including 2 pcs. Summation CTs)		L				
Primary rated current	1 A		1			
	5 A		5			
Secondary rated current	1 A		1			
	5 A		5			
none					*	
Latching relay and manual reset					<b>SP</b>	
none					*	
Extra equipment for reliable functioning during CT saturation <sup>1</sup>					<b>SAT</b>	

\* Please leave box empty if option is not desired

**Setting-list XD1-L**

Project: \_\_\_\_\_ SEG job.-no.: \_\_\_\_\_

Function group: = \_\_\_\_\_ Location: + \_\_\_\_\_ Relay code: - \_\_\_\_\_

Relay functions: \_\_\_\_\_ Date: \_\_\_\_\_

**Setting of parameters**

Function		Unit	Default settings	Actual settings
Id1	Differential current	% In	10	
Id2	Differential current	% In	10	





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